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Amendments to the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application.

1-45. Cancelled.

46. (new) A process for producing linear alkyl benzene, the process including the steps of obtaining a hydrocarbon condensate containing olefins, paraffins and oxygenates from a low temperature Fischer-Tropsch reaction;

- a) fractionating a desired carbon number distribution from the hydrocarbon condensate to form a fractionated hydrocarbon condensate stream which is the product of a Fischer-Tropsch reaction;
- b) extracting oxygenates from the fractionated hydrocarbon condensate stream from step (a) to form a stream containing olefins and paraffins which is the product of a Fischer-Tropsch reaction;
- c) combining the stream containing olefins and paraffins from step (b), which is the product of a Fischer-Tropsch reaction, with the feed stream from step (g) to form a combined stream;
- d) alkylating olefins in the combined stream from step (c) with benzene in the presence of a suitable alkylation catalyst in an alkylation reactor;
- e) recovering linear alkyl benzene from the alkylation reactor;
- recovering unreacted paraffins from the alkylation reactor; f)
- dehydrogenating the unreacted paraffins in the presence of a suitable g) dehydrogenation catalyst to form a feed stream containing olefins and paraffins; and
- h) sending the feed stream containing olefins and paraffins from step (g) to step (c).
- 47. (new) A process according to claim 46, wherein, in the extraction step b), the ratio of olefins to paraffins is substantially preserved.
- (new) A process according to claim 46, wherein the low temperature Fischer-48. Tropsch reaction is carried in a slurry bed reactor at a temperature of 160°C - 280°C and in the presence of a cobalt catalyst to provide a hydrocarbon condensate containing 60 to 80% by weight paraffins and 10 to 30% by weight olefins.

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49. (new) The process according to claim 48, wherein the Fischer-Tropsch reaction is carried out at a temperature of 210°C - 260°C.

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- 50. (new) The process according to claim 46, wherein the Fischer-Tropsch reaction is carried out in the presence of a cobalt catalyst.
- 51. (new) The process according to claim 48, wherein the hydrocarbon condensate contains less than 25% by weight olefins.
- 52. (new) The process according to claim 48, wherein the olefins in the hydrocarbon condensate have a linearity of greater than 92%.
- 53. (new) The process according to claim 52, wherein the olefins in the hydrocarbon condensate have a linearity of greater than 95%.
- 54. (new) The process according to claim 48, wherein the paraffins in the hydrocarbon condensate have a linearity greater than 92%.
- 55. (new) The process according to claim 46, wherein the hydrocarbon condensate is fractionated, in step a), into the C_8 to C_{16} range.
- 56. (new) The process according to claim 55, wherein the hydrocarbon condensate product is fractionated, in step a), into the C_{10} to C_{13} range.
- 57. (new) The process according to claim 56, wherein the fractionated hydrocarbon product contains 10 to 30% by weight olefins with a degree of linearity greater than 92%.
- 58. (new) The process according to claim 46, wherein the oxygenates are extracted, in step (b), by distillation, dehydration or liquid-liquid extraction.
- 59. (new) The process according to claim 58, wherein the oxygenates are extracted by liquid-liquid extraction.
- 60. (new) The process according to claim 59, wherein a light solvent is used in the liquid-liquid extraction.
- 61. (new) The process according to claim 60, wherein the light solvent is a mixture of methanol and water.

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62. (new) The process according to claim 61, wherein the oxygenate extraction process is a liquid-liquid extraction process that takes place in an extraction column using a mixture of methanol and water as the solvent, wherein an extract from the liquid-liquid extraction is sent to a solvent recovery column from which a tops product comprising methanol, olefins and paraffins is recycled to the extraction column, thereby enhancing the overall recovery of olefins and paraffins.

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- 63. (new) The process according to claim 62, wherein a bottoms product from the solvent recovery column is recycled to the extraction column.
- 64. (new) The process according to claim 61, wherein the solvent has a water content of more than 3% by weight.
- 65. (new) The process according to claim 64, wherein the solvent has a water content of from 5% 15% by weight.
- 66. (new) The process according to claim 62, wherein a raffinate from the extraction column is sent to a stripper column from which a hydrocarbon feed stream containing more than 90% by weight olefins and paraffins and less than 0.2% by weight oxygenates exits as a bottoms product.
- 67. (new) The process according to claim 66, wherein the hydrocarbon feed stream contains less than 0.02% by weight oxygenates.
- 68. (new) The process according to claim 46, wherein the recovery of olefins and paraffins in the hydrocarbon feed stream over the extraction step b) is in excess of 70%.
- 69. (new) The process according to claim 68, wherein the recovery of olefins and paraffins in the hydrocarbon feed stream is in excess of 80%.
- 70. (new) The process according to claim 46, wherein the olefin/paraffin ratio of the fractionated hydrocarbon condensate stream a) is substantially preserved over the extraction step b).
- 71. (new) The process according to claim 46, wherein the dehydrogenation reaction at step (g) is carried out at a conversion rate of 10%-15%.

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72. (new) The process according claim 71, wherein the fractionated hydrocarbon condensate from step (b) has an olefin concentration of from 10% to 30% by weight, the feed stream from step (g) has an olefin concentration of 10% to 15% by weight, and the combined stream at step (c) has an olefin concentration of 12.5% to 22.5% by weight.

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